

Analysis and Design of Airport Hangar

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Abstract— This paper describes about the planning, analysis and design of portable frame hangar to be built at Chennai. Normally lot of internal space is required for hangar, so it is preferable to build a portal frame. In this project analysis will be done both manually and by using STAADPro. The following components will be designed as per IS Standards Roof truss, purlin, columns, bases and footing will be designed. The hangar to be designed is a “FREE STANDING AIRCRAFT HANGAR”.

Keywords: Airport Hangar, Plastic Analysis, STAADPro

I. INTRODUCTION

A. General:

A hangar is a closed building structure to hold aircraft or spacecraft. Hangars are used for protection from the weather, direct sunlight, maintenance, repair, manufacture, assembly and storage of aircraft, aircraft carriers and ships. The primary function of a hangar is to provide an enclosure for servicing overhauling and doing repairs of the aircrafts. They are usually constructed of steel frames and covered with galvanised iron sheets. The shape of a hangar should be such that it covers minimum land area and yet provides adequate space for storage and comfortable manoeuvring of aircrafts.

II. AIRCRAFT HANGER DIMENSIONS AND LAYOUT

A. Aircraft Dimension:

Boeing 747-200
 Length = 68.6m
 Height = 19.6m
 Width = 59.6m

1) Hanger Dimension:

Length = 68.6m
 Consider single bay as 6m
 Provide 6 bays
 12 x 6m = 72m
 Provide length = 72m
 Height = 19.6 + Free board
 = 19.6 + 2.4
 Height = 22m
 Width = 3.2 + 59.6 + 3.2 (3.2m as clearance)
 Width = 66m
 Type of truss = Howe roof truss (North light roof truss)

B. Layout of Aircraft Hanger

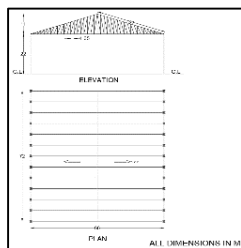


Fig. 1: Layout of aircraft hangar

III. DESIGN CALCULATIONS

A. Total Load Acting on Truss:

Dead load W = 4 KN
 W / 2 = 2 KN
 Live load W = 5.75 KN
 W / 2 = 2.875 KN
 Wind load W = 23.25 KN
 W / 2 = 11.625 KN

B. Design of Purlin

1) Bending Moment:

$M_{xx} = 11.34 \text{ KNm}$
 $M_{yy} = 3.78 \text{ KNm}$
 ISMC 200
 $Z_p = 141.372 \times 10^3 \text{ mm}^2$ (Required)
 Provided $Z_p = 181.6 \times 10^3 \text{ mm}^2$ (From steel table)
 $Z_p \text{ Required} < Z_p \text{ Provided}$
 $141.372 \times 10^3 < 181.6 \times 10^3$
 Hence safe

2) Section Classification:

$b_f / t_f = 75 / 11.4 = 6.5 < 9.4$
 $d_w / t_w = 165 / 6.1 = 27.04 < 42$
 Hence the section is plastic

C. Design of Truss Member

1) Data's to be collected for tension force:

Tension force T = 666.124 KN (member: 1750)
 For ISA 180 X 180 X 15 Single angle

2) Gross section yielding:

$T_{dg} = A_g \times F_y / \gamma_{m0}$
 $T_{dg} = 1176.13 \text{ KN} > 666.124$
 Hence safe

3) Net section Rupture:

$T_{dn} = 0.9 A_{nc} F_u / \gamma_{m1} + \beta A_{go} F_y / \gamma_{m0}$
 $T_{dn} = 1569.69 \text{ KN} > 666.12 \text{ KN}$
 Hence safe

4) Block shear criteria:

$T_{db1} = A_{vg} F_y / \sqrt{3} \times \gamma_{m0} + 0.9 A_{tn} F_u / \gamma_{m1}$
 $T_{db2} = 0.9 A_{vn} F_u / \sqrt{3} \times \gamma_{m1} + A_{tg} F_y / \gamma_{m0}$

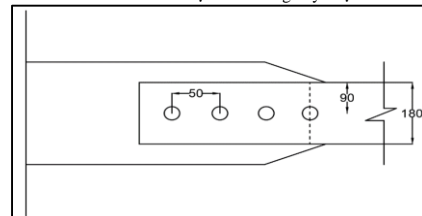


Fig. 2: Bolted connection

$T_{db1} = 712.958 \text{ KN} > 666.124 \text{ KN}$

$T_{db2} = 706.63 \text{ KN} > 666.124 \text{ KN}$

Hence safe

5) Data's to be collected for compression force:

Compression force = 851.214 KN (member 1751)
 For ISA 200 X 150 X 18

Single angle

6) Design compressive load:

$$P_d = A_e F_{cd}$$

$$P_d = 1284.2 \times 10^3 \text{ N} > 851.214 \text{ KN}$$

Hence safe

D. Design of Column

1) Data's to be collected:

$$P = 243.28 \text{ KN}$$

For section ISWB 500

2) Buckling class:

$$h / b_f = 500 / 250$$

$$= 2 > 1.2$$

$$t_f = 14.7 < 40$$

Hence the column belongs to Buckling class

'a' about zz axis

'b' about yy axis

$$P_d = F_{cd} A$$

$$P_d = 2562 \text{ KN} > 243.285 \text{ KN}$$

Hence safe

By interpolation for class 'b'

$$P_d = F_{cd} A$$

$$P_d = 584.28 \text{ KN} > 243.285 \text{ KN}$$

Hence safe

E. Design of Base Plate

Projected area

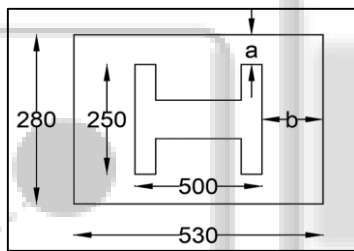


Fig. 3: Column located on base plate

$$a = 280 - 250 / 2$$

$$= 15 \text{ mm}$$

$$b = 530 - 500 / 2$$

$$= 15 \text{ mm}$$

1) Thickness of base plate:

$$t_s = 2.10 \text{ mm}$$

$$t_s \geq t_f$$

$$2.10 \text{ mm} \geq 14.7 \text{ mm}$$

So, provide 15mm thickness of base plate

Connecting 530 x 280 x 15mm base plate to concrete foundation

Use 4 Nos of 20mm ϕ of anchorage bolt @ 500mm length

2) Connection details:

When the column hence a base plate having been cutter by machine for perfect bearing load from the column will be transfer to base plate by using weltd connection.

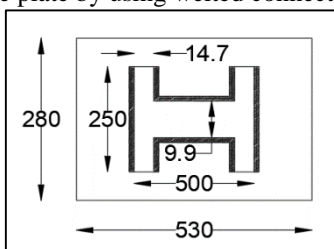


Fig. 4: Weltd connection

$$\text{Total length available} = 2 (250 + 250 - 9.9 + 500 - 14.7) = 1950.8 \text{ mm}$$

$$\text{Strength of weld} = 410 / \sqrt{3} \times 1 / 1.25 = 189.37 \text{ N/mm}^2$$

$$\text{The effective area of weld} = 0.7 t L_e p = 0.7 \times 4 \times L_e \times 189.37 = 378.641 \times 10^3$$

$$\text{Use 4mm weld } L_e = 714.09 \text{ mm} < 1950.8 \text{ mm}$$

Hence safe provide 4mm weld

F. Design of Footing

1) Check for one-way shear:

$$\tau_v = V_u / bd$$

$$V_u = q_a b [B / 2 - L / 2 - d]$$

$$q_a = 94.44 \times 1.5$$

$$q_a = 141.66 \text{ KN/m}^2$$

$$V_u = 0.14166 (b) [2100 / 2 - 550 / 2 - d]$$

Assume percentage of steel as 0.15%

$$\tau_v = V_u / bd$$

$$= 0.141 (b) [1050 - 275 - d] / b d$$

Consider τ_c as τ_v

$$\tau_c = 0.28 \text{ for } 0.15\% \text{ of steel}$$

$$0.28 d = 0.14 (1050 - 255 - d)$$

$$0.28 d = 111.3 - 0.14 d$$

$$d = 270 \text{ mm}$$

$$D = 325 \text{ mm}$$

2) Two-way shear (punching shear):

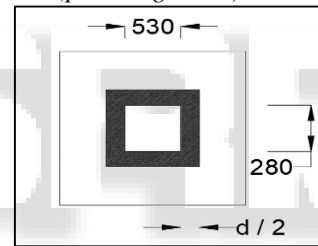


Fig. 5: Punching shear in footing

$$L_p = 2[d / 2 + d / 2 + 530] + 2[d / 2 + d / 2 + 280]$$

$$L_p = 2700 \text{ mm}$$

$$\text{Permissible stress} = 0.25 \sqrt{F_{ck}}$$

$$= 0.25 \times \sqrt{30}$$

$$= 1.36 \text{ N/mm}^2$$

$$0.57 \text{ N/mm}^2 < 1.36 \text{ N/mm}^2$$

Hence safe

3) Reinforcement calculation:

$$A_{st} = P_t b d / 100$$

$$= 0.07 / 100 \times 1000 \times 270$$

$$A_{st} = 189 \text{ mm}^2$$

$$\text{Minimum percentage of steel} = 0.12\% \text{ of } bD$$

$$= 0.12 / 100 \times 1000 \times 325$$

$$A_{st} = 390 \text{ mm}^2$$

$$a_{st} = \pi / 4 \times 10^2$$

$$= 78.5 \text{ mm}^2$$

$$\text{Spacing} = a_{st} / A_{st} \times 1000$$

$$= 78.5 / 390 \times 1000$$

$$\text{Spacing} = 201 \text{ mm} \sim 200 \text{ mm}$$

Provide 200mm C/C spacing of 10mm ϕ of bar

IV. PLASTIC ANALYSIS

A. Beam Mechanism:

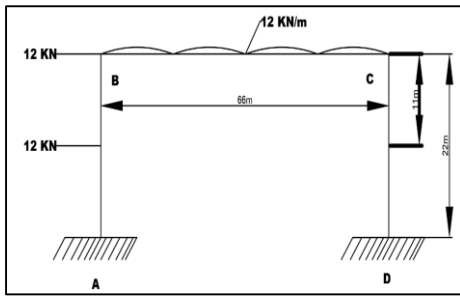


Fig. 6: Beam Mechanism

$M_p = 2178 \text{ KNm}$

B. Column Mechanism:

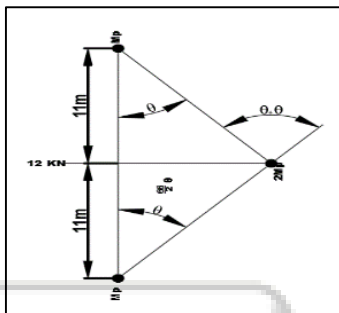


Fig. 7: Column Mechanism

$M_p = 22 \text{ KNm}$

C. Sway Mechanism:

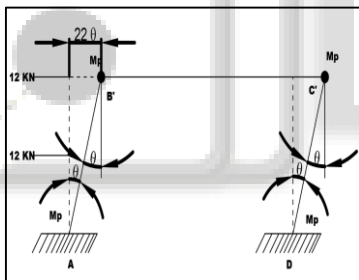


Fig. 8: Sway Mechanism

$M_p = 99 \text{ KNm}$

D. Combined Mechanism:

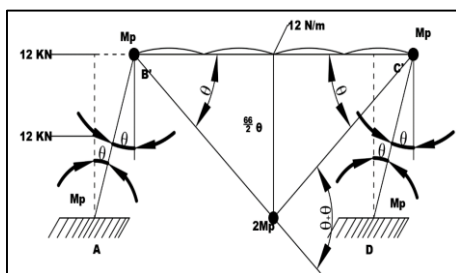


Fig. 9: Combined Mechanism

$M_p = 1683 \text{ KNm}$

Hence the plastic moment of resistance, $M_p = 2178 \text{ KNm}$

V. STAAD PRO ANALYSIS

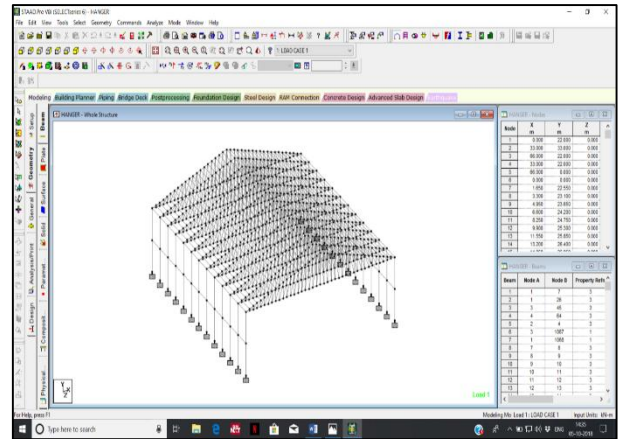


Fig. 10: Modelling of hangar

Job No. Sheet No. 1 Rev.

Job Title: Software licensed to H*

Client: HANGER.std

STAAD.Pro Query Property
Beam no. 1915

Section: ISWB500

Length = 11

Unit: kN - m

Physical Properties

Ax	0.012	Ix	0.000
Ay	0.005	Iy	0.000
Az	0.005	Iz	0.001
Depth	0.500	Width	0.250

Material Properties

Elasticity(kN/mm ²)	205.000	Density(kg/m ³)	76.820
Poisson	0.300	Alpha	12 E-6

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STAAD.Pro V8i (SELECT series 6) 20.07.11.33

Fig. 11: Property

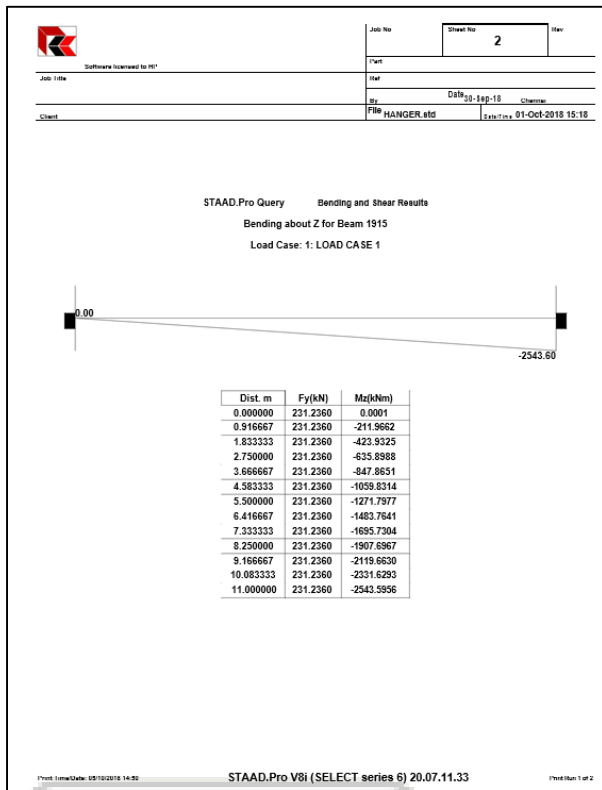


Fig. 12: Bending and Shear Results

VI. STAAD PRO DESIGN RESULTS

Group No	Group Name	Member number	Original section	Design section	Member spec	Slenderness check	Axial check	combination of axial & bend check	Shear along y check	Shear along z check
G1	Design Grid	M1	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M2	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M3	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M4	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M5	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M6	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M7	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M8	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M9	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M10	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M11	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M12	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M13	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M14	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M15	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M16	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M17	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M18	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M19	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M20	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M21	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M22	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS
		M23	ISW 8500	ISW 8500	BEAM	PASS	N/A	PASS	PASS	PASS

Table 1:

VII. CONCLUSION

In our project we have analyzed and designed “Free standing aircraft hangar” both in staad pro as well as manually based on the dimensions of “Boeing 747-200” aircraft. From this project we have learnt that for a portable frame structure free standing hangar is suitable. This project we have designed steel structures such as truss, purlin, column, beam, and base plate from code books of IS standards on Indian conditions. So overall comparing manual calculations and staad pro out puts staad pro analysis and design is more essential and time saving and more over all sections for beams and columns are automatically selected by the software based on best preference or satisfying all conditions economically. We have learnt how to make use of code books to design steel structures and how to complete a project.

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