

Improving Thermal Withstanding Capacity of Single Phase Induction Motor Using NWCC Method

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Abstract— Single phase induction motors are extensively used for smaller loads in industries and domestic purposes due to their various technical as well as economical advantages. Temperature rise due to heat dissipation caused by various losses inside the motor is a critical factor which degrades the dielectric properties of insulation and shortening the lifespan of motor. This paper presents the capillary based water cooling method of single phase squirrel cage induction motor. In this method, a jacket of capillaries made of jute and cotton is used as an outer cover for the motor casing. A small air gap passage is provided in between motor casing and inner surface of jacket. Natural Water Cooling Capillaries (NWCC) method is used to lower down the surrounding temperature of motor which reduces thermal limitations of motor. For this purpose we select a 0.37 kW single phase, 50Hz squirrel cage induction motor. Heat run test is performed to determine the total loss of energy dissipated as heat on single phase squirrel cage induction motor with and without adopting capillary based water cooling method. Comparison is done on the basis of experimental result which shows that the temperature withstanding capacity of induction motor will increase by 10.67 % after adopting capillary based water cooling method. This is an economical method and no external energy is required for cooling purpose.

Key words: Capillaries, Heat run test, Squirrel cage induction motor, Temperature withstanding capacity, Water cooling

I. INTRODUCTION

Single phase induction motors are widely used in small industrial applications, domestic applications like fans, centrifugal pumps, blowers, lifts, washing machines, and so on. Most of the motors are not only used in fixed-speed load services but also used in variable frequency drive (VFD) services, variable torque centrifugal pumps, fans, and compressor loads. The pay-off for that will be an increase in operating temperature conditions [1]. All electrical rotating machines generate heat as a result of electrical and mechanical losses inside it. Rise in temperature due to heat is one of the sources of increased stress on induction motor's insulation [2]. There is a well known fact that the operating temperature of an electric machine has a very strong relationship with the life duration of insulation and both are inversely proportional [3] So, cooling is necessary for continuous heat removal from motors. Most commonly used motors are Totally Enclosed Fan Cooled (TEFC) type which is provided with an external forced air cooling fan mounted on the Non-Driven End (NDE) of the shaft with cooling ribs running axially along the outer surface of motor frame [4]. Some limitations of this type of air cooling systems are- TEFC type air cooling is effective only along the axis of rotor but it cannot remove the motor's surrounding heat and the heat transfer coefficient of air is

too low to reduce excessive heat from stator's fin. With increase in motor's power rating, dimension of rotor increases but heat removal rate decreases [5].

To achieve a higher power to dimension ratio, a highly effective cooling and ventilation system is required which can ensure sufficient heat removal from the inner side of motor. Substantial improvement can be achieved by adopting direct water cooling methods which ensure relatively low temperature of stator. Following water cooling techniques for induction motor are usually in practice:

- (1) Water cooled model for induction motor using thermography technique [6].
- (2) Totally enclosed water cooled method for squirrel cage induction motor [7].
- (3) Twin water cooled wheel design for cooling of induction motor [8].
- (4) Forced cooling by stator mounted water pipes [5].

The above four methods are forced water cooling methods which requires external energy for functioning. While in this paper, the thermal withstanding capacity of a single phase induction motor is improved by using Natural Water Cooling Capillaries (NWCC) method which does not require big external heat exchanger as well as external energy for cooling. Water absorbed by capillaries creates natural ventilation system which lower down the temperature of motor's surrounding. Materials and methods adopted are described in section 4 and experimental results are discussed in section 5.

II. MECHANISMS OF HEAT GENERATION INSIDE AN ELECTRICAL INDUCTION MOTOR

All rotating electrical machines dissipate heat as a result of electrical and mechanical losses, inside the machines. Losses are higher during the process of starting of motor and dynamic braking and are increases with loading [9]. The mechanism of heat generation in induction motors are classified into four groups, mainly related to the places where losses occur. These are joule losses, iron losses, stray losses and mechanical losses [10].

A. Joule Losses:

This mechanism corresponds to the conversion of electrical energy into thermal energy. These types of losses are directly related to electric resistance of the conductor and changes proportionally to the square of the current which is represented by equation as [11]:

$$P_j = I^2 * R$$

Energy conversion by joule effect in squirrel cage induction electric motors occurs in the stator (copper windings) and in the squirrel cage (aluminium bars).

B. Iron Losses:

These losses are due to the conversion of electric energy into thermal energy in the iron. They are divided in the hysteresis and Foucault (eddy currents) losses. The eddy current losses are joule losses that occur in the flow of an induced electric current. The hysteresis losses are due to the energy expended to align the iron magnetic poles to the applied magnetic field [12].

C. Stray Load Losses:

The stray load losses are minor losses in the electric motor operation and their quantification is very difficult [13]. This includes the losses due to the skin effect, high frequency among others that remains constant.

D. Mechanical Losses:

These losses comprise the conversion of the mechanical energy into thermal energy due to mechanical friction. Here includes mainly the losses due to rolling bearings (ball/ring interface) and the cooling fan losses.

III. HEAT TRANSFER MECHANISMS IN INDUCTION MOTOR

The transfer mechanism of heat, which is generated as a result of various losses in motor, is discussed here. All three main transfer mechanisms conduction, convection and radiation are involved in the heat exchange of single phase squirrel cage induction motor is described below.

A. Conduction:

In the solid part of motors such as rotor and stator, heat is typically transferred by conduction. It is an energy transferred due to the temperature difference by the mechanism of intermolecular interactions. The flow of heat by conduction occurs via collision between atoms and molecules and subsequent transfer of kinetic energy [14]. Hence, for this part standard Fourier's law is used to connect the heat flux and the temperature gradient, given by equation as:

$$Q = \lambda A \nabla T$$

Where Q presents heat flow, λ is the thermal conductivity of material, A is surface area and ∇T is temperature gradient.

B. Convection:

It is an energy transferred due to temperature difference because of combined mechanisms of intermolecular interactions and bulk transport of heat in air medium. This temperature difference will cause force convection on the frame of motor where the air does not flow on its own but it is rather pushed. There are other parts of motor where convection mode for the energy transfer is used as heat transfer in the air gap, from shaft, from the rotor, shaft ends, magnetic bearings in the cooling duct, and in the end winding space [15]. The expression for the flux of such forced convection is given in the form:

$$Q = \alpha A_s \Delta T$$

Where α presents heat transfer coefficient, A_s is the surface area from which convection is occurring and ΔT defines temperature difference.

C. Radiation:

A part of heat in induction motor is transferred by radiation. The actual amount of energy transferred in the form of electromagnetic waves depends not only on the emissivity properties of a part of the motor under consideration, but also on the temperature itself. Due to the temperature difference between the motor surface and the ambient temperature, the heat will be radiated out from the whole of motor surface and the energy radiated can be evaluated according to the Stefan – Boltzmann law of radiation [16]:

$$Q = \varepsilon \sigma A (T_s^4 - T_{sur}^4)$$

ε presents surface emissivity, σ is Stefan-Boltzmann constant and its value is $5.67 \cdot 10^{-8} \text{ W/m}^2\text{K}^4$, T_s is the temperature of surface and T_{sur} is the temperature of surroundings.

IV. EFFECT OF HEAT ON THERMAL WITHSTANDING CAPACITY OF INDUCTION MOTOR

The major issue which shortens the motor's life is heat. The insulation type used in an electric motor depends on the temperature at which motor will operate. Every insulating material has a certain working temperature complying with the expected life of the motor and allowing it to safely function within this expected period. Even a small increase in temperature can considerably decrease the working life of insulating material. According to the 10^0 C rule, the life of insulation system is halved for each additional 10^0 C in the temperature at which it is exposed [17].

According to IEC 60085 standards, the insulating materials used in electric motors can be classified into four thermal classes that are class A, class B, class F and class H. Fig. 1 shows the reduction of life of insulation system in hour verses the temperature rise by means of thermal classification of insulating materials used. Proper cooling techniques must be chosen and working temperature of certain parts of motor must be stable.

V. MATERIALS AND METHODS

This section provides an overview of experimental setup of NWCC method. For this purpose a single phase induction motor and its specifications are given in table 1.

Most of the losses occur in the stator part of motor and this is the major source of heat dissipation. By the conduction, convection and radiation modes of heat transfer, heat reaches to the outer casing of motor and is uniformly distributed which results in rise in temperature of surrounding. NWCC method is used to reduce this temperature and acts as a safeguard for the protection of insulation material, to increase the thermal withstanding capacity as well as life of motor. In this method, a capillary jacket is used which is placed above the casing of motor. Fig. 2 shows the structure of capillary jacket which is a hollow cylindrical structure, its inner layer is made by porous mat of tatties matrix (used in evaporative coolers) and capillary tube which is a cylindrical pipe composed of capillaries made of cotton and jute.

Capillary jacket is comprised of three layers. First layer is of Tatties matrix which has a property of high temperature withstanding capability. So, its main function is to protect the jacket's capillaries from overheating of motor and also provide structural support. Middle layer of jacket is

made of cotton material which is wrapped on the layer of tatties matrix. Main function of middle layer is to provide uniformity to capillary effect. Top most layer of jacket is of capillary structure. Capillaries are made by jute and cotton materials which are attached on the outer surface of jacket. Composition of jute fibre [18] is given in table 2.

When water flows through these capillaries, water molecules are absorbed by cotton and jute material, due to their structure and chemical nature. In order to reduce the surrounding air temperature of working motor, the quantity of water absorbed by the capillaries differs with time which is shown in table3.

Fig. 3 shows the working of NWCC method applied on single phase induction motor. Funnel is used to transfer water from storage tank which can be managed through tap arrangement. Funnel is joined with a bunch of capillary tubes and same capillaries are attached to the outer surface of jacket. Inlet water from capillary tube is uniformly distributed in the capillaries of jacket through absorption process. Water is further absorbed by the layer of cotton which cools the passage of air in between motor casing and jacket. Natural cooling phenomenon takes place when passage air molecules come in contact with the wet layer of jacket; simultaneously there is reduction of surrounding temperature. This heat removal process from motor is beneficial for improving the temperature withstanding capacity of motor as well as life of insulation used.

VI. RESULT AND DISCUSSION

A. Heat Run Test:

This test is done on single phase squirrel cage induction motor to determine the part of input energy which is dissipated as heat due to the losses. Heat run test is conducted on the motor as per IEC 60851. Temperature of motor stator winding is measured with standard digital temperature indicator. Tests were conducted on the motor with applying NWCC method and without NWCC method. Table 4 shows the temperature of stator winding in both cases with respect to time.

Fig. 4 shows the graphical comparison of temperature variation of stator when test is performed with and without NWCC method. The result shows that there is satisfactory performance of NWCC method and temperature is reduced by 8°C.

Perhaps increase in thermal withstanding capacity of single phase induction motor by adopting NWCC method from experimental result performed on it, for 40 minutes can be determined as follows.

$$\frac{(T_{without} - T_{with}) * 100}{T_{without}}$$

$T_{without}$ presents final temperature of motor without applying NWCC method in °C, T_{with} presents final temperature of motor with applying NWCC method in °C

$$= \frac{(58.1 - 51.9) * 100}{58.1} = 10.67\%$$

This shows that the thermal withstanding capacity of single phase induction motor is increased by 10.67%.

VII. FIGURES AND TABLES

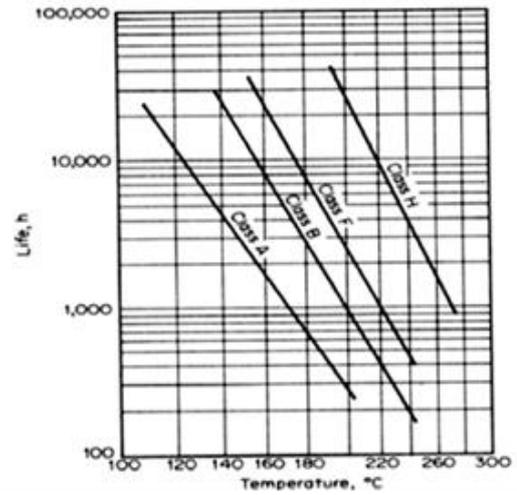


Fig. 1: Insulation life versus temperature rise.

Parameters	Ratings
Power	0.37 kW
Speed	1500 rpm
Current	4 A
Voltage	230 V
Frequency	50 Hz

Table 1: Specification of Single Phase Induction Motor



Fig. 2: Structure of capillary jacket and capillary tube

Composition	Weight in percentage (%)
Lignin	12-14
α- cellulose	58-63
Hemicelluloses	21-24
Minor constituents	2-4

Table 2: Composition of Jute Fibre

Time of operation of single phase induction motor (minutes)	Quantity of water absorbed by capillaries (ml)
40	450
60	675
120	1350
80	2025

Table 3: Quantity of Water Absorbed By the Capillaries with Time

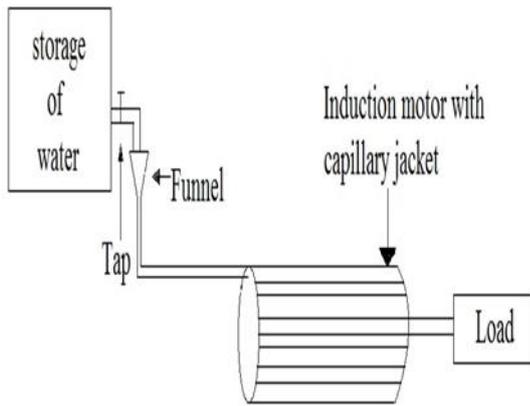


Fig. 3: working of NWCC method

Time in minutes	Temperature (°C) of motor without NWCC method	Temperature (°C) of motor with NWCC method
0	28.5	28.4
2	31.6	30.5
4	34.4	32
6	36.3	33.1
8	38.1	34.2
10	39.7	35.4

12	41.1	36.8
14	42.6	38.1
16	44	39.3
18	45.2	40.6
20	46.2	41.5
22	47.5	42.6
24	48.7	43.8
26	49.8	44.7
28	51.1	45.8
30	52.2	46.8
32	53.1	47.5
34	54	48.3
36	55.1	49.2
38	56.3	50.2
40	58.1	51.9

Table 4: Temperature Of Stator (With And Without Using NWCC Method) With Respect To Time.

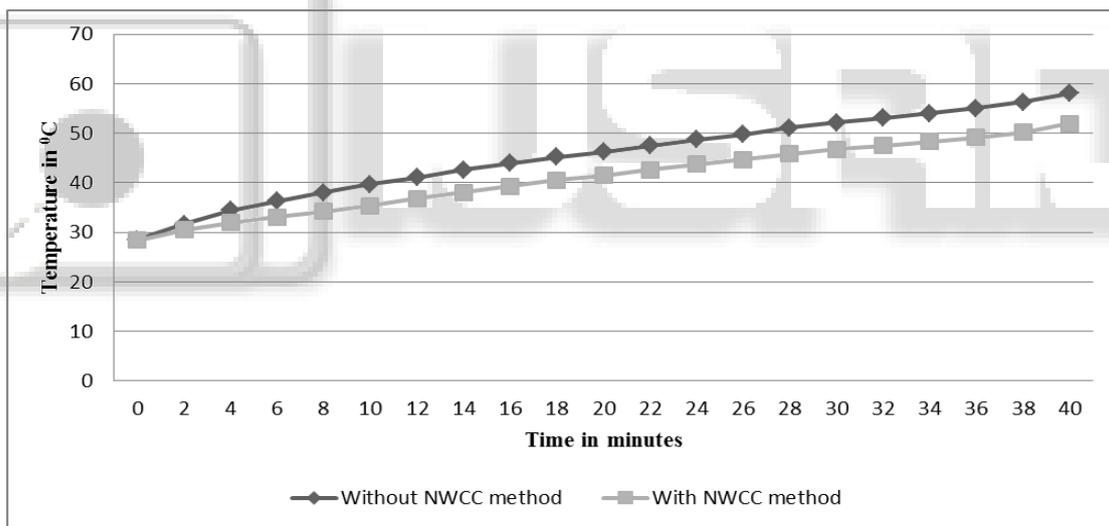


Fig. 4: Temperature variation of stator with and without NWCC method

VIII. CONCLUSION

In this paper, the stator and core temperature of a 0.37kW single phase squirrel cage induction motor is lowered by means of NWCC method. It is shown that when NWCC method is applied, the stator temperature decreases which increases the thermal withstanding capacity of insulation as well as life of motor. The impact of cooling on the thermal withstanding capacity of the motor was presented and by experimental analysis it is increased by 10.67%.

It should be noted that the method used in this paper is of low cost and consumes less water. It does not require any external energy for cooling. Materials used to prepare apparatus for this method are easily available.

NWCC method is highly effective due to high specific heat capacity of water and high heat transfer coefficients.

IX. REFERENCES

- [1] R.Beguenane and M.E.H.Benbouzid, "Induction motors thermal monitoring by means of rotor resistance identification", IEEE Transactions on Energy Conversions, vol. 14(3), pp. 566-570, 1999.
- [2] Mendes, A.M.S., Lopez Fernandez, X.M. and Marques Cardoso, A.J., "Thermal performance of a single phase induction motor under fault tolerant operating strategies", IEEE Transactions on Power Electronics, vol. 23(3), pp. 1537-1544, 2008.

- [3] E.L. Brancato, "Estimating the lifetime expectancies of motors", IEEE Electrical Insulation Magazine, vol. 8(3), pp. 5-13, 1992.
- [4] K.G. Bante, S.G. Tarnekar and D.R. Tutakane, "AC motor cooling system analysis based on application case study", International Journal of Engineering Inventions, vol. 2(8), pp. 9-15, 2013.
- [5] M. Sikora, R. Vilach and P. Navratil, "The unusual water cooling applied on small asynchronous motor", Engineering Mechanics, vol. 18(2), pp. 143-153, 2011.
- [6] S.S. Borges, C.A. Cezario and T.T. Kunz, "Design of water cooled electric motors using CFD and thermography techniques", ICEM 2008, Proc. 18th International Conference on Electrical Machines, Vilamoura, 2008.
- [7] C. Kral, A. Haumer and T. Bauml, "Thermal model and behaviour of totally enclosed water cooled squirrel cage induction machine for traction applications", Industrial Electronics, vol. 55(10), 2008.
- [8] F. Caricchi, F. Crescimbin, A. Di Napoli and M. Marcheggiani, "Prototype of electric vehicle drive with twin water cooled wheel direct drive motors", Proc. 27th Annual IEEE, Power Electronics Specialists Conference, Baveno, 1996.
- [9] S.L. Ho and W.N. Fu, "Analysis of indirect temperature rise test of induction machine using time stepping FEM", IEEE Transactions on Energy Conversions, vol. 16(1), pp. 55-60, 2001.
- [10] T.F. Chan, "A method to determine the temperature rise of induction motors", International Journal of Electrical Engineering Education, vol. 27, pp. 45-52, 1990.
- [11] R. Findlay, N. Stranges and D.K. Mackay, "Losses due to rotational flux in three phase induction motor", IEEE Transactions on Energy Conversions, vol. 9, pp. 543-549, 1994.
- [12] C. A. Hernandez-Aramburo, T. C. Green and A.C. Smith, "Estimating rotational iron losses in an induction machine", IEEE Transactions on Magnetism, vol. 39(6), pp. 3527-3533, 2009.
- [13] C. A. Hernandez-Aramburo, T. C. Green, and A. C. Smith, "Assessment of power losses of an inverter-driven induction machine with its experimental validation", IEEE Transaction on Industrial Applications, vol. 39, pp. 994-1004, July-Aug. 2003.
- [14] L.I. Zhu and X.J. Zheng, "A theory for electromagnetic heat conduction and numerical model based on boltzmann equation", International Journal of Nonlinear Science and Numerical Simulation, vol. 7(3), pp. 339-344, 2006.
- [15] Y. Huai, R.V.N. Melnik and P.B. Thogersen, "Computational analysis of temperature rise phenomena in electric induction motors", Applied Thermal Engineering, vol. 23(1), pp. 779-795, 2003.
- [16] R. Siegel and J.R Howell, "Thermal radiation heat transfer", 3rd ed., Hemisphere Publication Co. Washington; 1992.
- [17] B. Baptista, A. Mendes, S. Cruz and A. Cardoso, "Temperature distribution inside a three phase induction motor running with eccentric air gap", Electrical Review, vol. 8(1), pp. 96-99, 2012.
- [18] R. Masoodi and K.M. Pillai, "A study on moisture absorption and swelling in bio-based jute-epoxy composites", Journal of Reinforced Plastics and Composites, vol. 31(5), pp. 285-292, 2012.